





# SST Analysis in NCEP GFS

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# **General Picture**

### --- SST Improvement

**Better SST Analysis Product** 

Extract SST information from satellite data more effectively

From Empirical retrieval to Physical retrieval to Direct assimilation of radiances Resolve the vertical structure from surface to diurnal warming depth

Enable to use depth dependent observations consistently

Require to solve new, related issues

# **Assimilation scheme**

- SST is analyzed with the atmospheric data assimilation system (GSI) in NCEP GFS
  - Add a new analysis variable (SST or equivalent) to GSI
    - Single cost function with more elements in the state vector
  - Add observation data related to SST
  - Error variance and correlation length for the new analysis variable

### • Problems

- SST prediction
- Observation operators (H) for the new analysis variable (x) are not available, if the observations (y) are depth dependent.
- Jacobi of the new observation operators need to be derived
- Different lower temperature condition required for atmospheric model (Ts) and radiative transfer model (Tr).

# **Observations for SST analysis**

Satellite: IR & MW The radiances emitted from the sea water at skin depths (0.01mm – 1 mm) In situ: Buoys, Ships The sea water temperature at the depths (0.01 mm - 15 + m)

# SST is not observed directly

(1) A various depths instead of surface (z = 0) only(2) Radiance instead of temperature

## Questions

Is it necessary to resolve the vertical structure near surface? How? How to assimilate the indirectly observed data?

#### Representative temperatures near sea surface and analysis variable



- $T_{ir}$  : Skin temperature, z ~ 0.01 mm. Detected by shortest IR (80000 GHz, CH-2 of AVHRR)
- $T_{mw}$  : Sub-skin temperature, z ~ 1.0 mm. Detected by longest MW (6.7 GHz, CH-1 of AMSRE)
- $T_r$  : Skin temperature, z ~ 0.01 mm 1.0 mm. Between  $T_{ir}$  and  $T_{mw}$
- $T_d$  : Depth Temperatures, z ~ 0.17m ~ 15m. Detected by buoys and ships
- $T_f$  : Foundation temperature,  $z = D_T$  ~ 0.5 m 10 m

### Analysis variable: Foundation temperature $T_f$ $T_s = f_s(T_f) = T_f + \Delta T_w(0) - \Delta T_c(0); T_r(\delta_r) = f_r(T_f) = T_f + \Delta T_w(\delta_r) - \Delta T_c(\delta_r)$ $T_{mw}(\delta_c) = f_{mw}(T_f) = T_f + \Delta T_w(\delta_c); T_d(d) = f_d(T_f) = T_f + \Delta T_w(d)$

### Sub-layer and diurnal warming layer

Sub-layer cooling model (Fairall et al , 1996):

$$-Q = R_{nl} - H_{s} - H_{l}$$

$$\delta_{c} = \frac{\lambda v}{(\rho_{a} / \rho)^{1/2} u_{*a}} = 6\{1 + \left[\frac{16 Q_{b} g \alpha \rho c_{p} v^{3}}{u_{*a}^{4} (\rho_{a} / \rho)^{2} \kappa^{2}}\right]^{3/4}\}^{-1/3} \frac{v}{(\rho_{a} / \rho)^{1/2} u_{*a}}$$

$$Q_{b} = Q + \left(\frac{S \beta c_{p}}{\alpha L_{e}}\right) H_{l}$$

$$\Delta T_{c} = \frac{H \delta_{c}}{\kappa} = \frac{6 v (\delta S_{w} - Q)}{\kappa (\rho_{a} / \rho)^{1/2} u_{*a}} \{1 + \left[\frac{16 g \alpha \rho c_{p} v^{3} \left(Q + \frac{S \beta c_{p}}{\alpha L_{e}}\right) H_{l}}{u_{*a}^{4} (\rho_{a} / \rho)^{2} \kappa^{2}}\right]^{3/4}\}^{-1/3}$$

**Diurnal warming model** (Fairall et al, 1996):

The model assumes linear anomaly profiles of temperature and current in the diurnal warming layer. Once the solar heating exceeds the combined cooling of sensible, Latent and long wave radiation, integrate temperature equation and current equations (rotation effect omitted) along time  $\begin{pmatrix} t_0 \rightarrow t \end{pmatrix}$  and depth  $\begin{pmatrix} 0 \rightarrow D_T \end{pmatrix}$ 

$$\Delta T_{w} = \frac{I_{h}}{\rho c_{p} (D_{T}/2)}; \quad \Delta \rho = \alpha \Delta T_{w}; \quad \delta V = \frac{2I_{\tau}}{D_{T}}; \quad I_{h} = \int_{t_{0}}^{t} (\delta S_{w} - Q) dt; \\ I_{\tau} = \int_{t_{0}}^{t} u_{*o}^{2} dt$$

Assume the density and current anomalies, which mean the departures from the early morning oceanic state, and length scale satisfy Richardson number criterion:

$$\frac{gh\delta\rho}{\rho_o(\delta V)^2} \ge R_{ic} = 0.65 \Longrightarrow D_T(t) = \sqrt{2R_{ic}} \frac{I_\tau}{\sqrt{(\alpha g / \rho c_p)I_h}}$$

#### **Observation operators from** $T_f$ **to** $T_d$ **and** $T_r$ **:**

Conventional data:  $T_d(d) = f_d(T_f) = T_f + \Delta T_w(d)$   $H_c(T_f) => T_f$   $H_c[f_d(T_f)] => T_d$ Satellite data:  $T_r(\delta_r) = f_r(T_f) = T_f + \Delta T_w(\delta_r) - \Delta T_c(\delta_r)$  $H_r(T_r) => T_r$ 

 $H_r[f_r(T_f)] \Longrightarrow T_r$ 

**Observation operator:** To transform analysis variable to corresponding partner in observation space.

 $H_c$ : available, interpolation operator

 $H_r$ : available, radiative transfer model

Conversion between SST  $(T_s)$  and  $T_r$ :

 $T_{s} = f_{s}(T_{f}) = T_{f} + \Delta T_{w}(0) - \Delta T_{c}(0) \quad H_{c}(T_{f}) \Longrightarrow T_{f}; H_{c}[f_{s}(T_{f})] \Longrightarrow T_{s}$ 

#### Sensitivities of the representative temperatures to $T_f$ :

 $\begin{array}{l} \textbf{Conventional data} \quad \frac{\partial T_d}{\partial T_f}:\\ T_d(d) = f_d(T_f) = T_f + \Delta T_w(d) \Longrightarrow F_d\{T_d, T_f, \Delta T_w[D_T(I_h(D_T, T_s)]\} = 0\\ F_d[T_d, T_f, \Delta T_w(T_s)] = 0 \Longrightarrow \frac{\partial T_d}{\partial T_f} = P_d(\frac{\partial \Delta T_w}{\partial T_s}, \frac{\partial T_s}{\partial T_{mw}}, \frac{\partial T_m}{\partial T_d})\\ \textbf{Satellite data} \quad \frac{\partial T_r}{\partial T_f}:\\ T_r(\delta_r) = f_r(T_f) = T_f + \Delta T_w(\delta_r) - \Delta T_c(\delta_r)\\ \Longrightarrow F_r[T_r, T_f, \Delta T_w(T_s) - \Delta T_c(T_s)] = 0\\ \Longrightarrow \frac{\partial T_r}{\partial T_f} = P_r(\frac{\partial \Delta T_w}{\partial T_s}, \frac{\partial T_s}{\partial T_r}) \end{array}$ 

 $F_d$ : Implicit compound function to relate  $T_d(z=d)$  and  $T_f$  through Heat fluxes and therefore  $T_s$ 



**Diurnal warming model run with 3-hourly GFS fluxes** 



Sub-layer model run with 3-hourly GFS fluxes



Sensitivities of representative temperatures to foundation temperature

Simulation of ocean diurnal warming and sub-layer cooling. 092, 02/03/2006 (3-hour warming integration with 3-hour mean fluxes, from 06Z, 02/03/2006)



#### **Experiment:**



Use the SST currently used by GFS,  $T_{ctl}$ as the foundation temperature. Satellite instruments are divided into IR and MW: For IR:  $T_{ir} = T_{ctl} + \Delta T_w (z = 0) - \Delta T_c (z = 0)$ 

For MW: 
$$T_{mw} = T_{ctl} + \Delta T_w (z = 0)$$

Then, 7-day analysis is done with GSI, GFS forecast (03, 06, 09) used as the first guess; GFS fluxes used to get  $\Delta T_w$  and  $\Delta T_c$ 

**Control Run**: 
$$T_{ir} = T_{mw} = T_{ctl}$$



AVHRR (NOAA-18) dTb (obs - rtm) & Nsamp (dTw - dTc) dependency. Without BC. Ges. Based on 3-day (02/13/2006 - 02/15/2006) 6-hourly samples.

Impacts of sea water diurnal warming and sub-layer cooling on AVHRR radiance simulation (Bias), based on the data used in both experiments

AVHRR (NOAA-18) dTb (obs - rtm) & Nsamp (dTw - dTc) dependency. With BC. Anl. Based on 3-day (02/13/2006 - 02/15/2006) 6-hourly samples.



# Plan

### • Foundation temperature analysis in GSI

- $-T_f$  error statistics based on a period of analysis sample
- How often the fluxes and therefore the diurnal warming amount updated?
- Parallel run
  - Consistency among SST, fluxes and atmosphere

### • Diurnal warming model improvement

- Theoretical analysis done: rotation effect, vanish wind handle, E-P effect, linear to exponent profile
- Solar radiation penetration

### One-dimensional oceanic model

 $-T_f$  forecasting